

CLAIM AMENDMENTS

1. (currently amended) A method comprising the steps of:
  - ~~(b)~~—initiating a seek to move a moveable arm from an initial position to a destination position;
  - (c)—receiving a position error signal indicative of a position of the moveable arm;
  - (d)—generating a compensation signal based on the position error signal, a loop matching and an oscillation frequency of the moveable arm and adapted to minimize a component of the position error signal arising from the oscillation frequency; and
  - (e)—applying the compensation signal to control the moveable arm as a feedforward signal as the moveable arm settles onto the destination position.
2. (currently amended) The method of claim 12, wherein the identifying step (a) comprises steps of abruptly accelerating and decelerating the actuator arm to subject the actuator arm to a broad spectrum excitation, and measuring the actuator arm oscillation resulting from the excitation.
3. (original) The method of claim 1, further comprising a step of entering a track following mode to cause the head to remain over the destination track while removing the compensation signal from the servo loop.
4. (currently amended) The method of claim 1, wherein the applying step (e) produces a notch in an error sensitivity function relating the position error signal to a moveable arm oscillatory disturbance.
5. (original) The method of claim 4, wherein the compensation signal is generated in accordance with the following relation:

$$A(z) = \frac{u_f}{PES} = \frac{z^2 \left[ \frac{\mu_0}{\alpha} \cos(\varphi) \right] - z \left[ \frac{\mu_0}{\alpha} \cos(\varphi + \omega_0 T) \right]}{\frac{z^2}{\eta} - z[2 \cos(\omega_0 T)] + \eta}$$

where  $u_{ff}$  is the compensation signal, PES is the position error signal,  $z$  is a  $z$  transform function,  $\omega_0$  is a nominal frequency of the notch,  $\eta$  controls a nominal depth of the notch,  $\mu_0$  controls a nominal width of the notch,  $\alpha$  is a gain parameter indicative of a closed loop gain of the servo loop at  $\omega_0$ ,  $\phi$  is a phase parameter indicative of a phase response of the servo loop at  $\omega_0$ , and  $T$  is a sampling period.

6. (currently amended) An apparatus comprising:
  - a controllable structure; and
  - a servo circuit coupled to ~~the~~ control the controllable structure, comprising:
    - a servo controller which controls position of the controllable structure in response to a position error signal indicative of a position of the controllable structure, the servo controller configured to perform a seek operation to move the controllable structure from an initial position to a destination position; and
    - a filter operably coupled in parallel with the servo controller to receive the position error signal and to generate a compensation signal during for a settle mode as the controllable structure is brought over the destination position, the compensation signal based on the position error signal, a phase response of at least the servo circuit and an unwanted oscillation frequency of the controllable structure induced by a resonance mode excitation during the seek, the compensation signal adapted to cancel a component of the position error signal arising from the unwanted oscillation frequency.
7. (original) The data handling system of claim 6, wherein the servo circuit further comprises:
  - a demodulator which generates the position error signal in response to servo data transduced by the head from the recording surface; and
  - a motor driver which applies a current to an actuator motor to move the actuator arm, wherein the servo controller generates a current command signal which is

combined with the compensation signal to generate a modified current command signal which is used by the motor driver to apply current to the actuator motor.

8. (original) The data handling system of claim 6, wherein the servo circuit determines the frequency of oscillation by abruptly accelerating and decelerating the actuator arm to subject the actuator arm to a broad spectrum excitation, and measuring the actuator arm oscillation resulting from the excitation.
9. (original) The data handling system of claim 6, wherein the filter comprises a second order, linear time-invariant filter with a trigonometric function based transfer function.
10. (original) The data handling system of claim 6, wherein the actuator assembly comprises a plurality of actuator arms each supporting at least one head, and wherein the filter is configured to independently compensate oscillation of each arm.
11. (canceled.)
12. (previously presented) The method of claim 1 further comprising the step of identifying the oscillation frequency of the moveable arm induced by a resonance mode excitation.
13. (currently amended) A method ~~comprising the step of~~ minimizing a frequency relative to a position error signal of a controlled system independent of whether the frequency is a resonance mode of the controlled system, wherein the minimizing is based in part on a loop matching.
14. (previously presented) The method of claim 13 that is further capable of minimizing a frequency relative to a position error signal of a controlled system, the frequency is not a resonance mode of the controlled system.
15. (currently amended) A method ~~comprising the step of~~ increasing a sensitivity of a control system at a frequency to minimize a frequency relative to a position error signal, wherein the increasing is based in part on a phase response of the control system.

16. (previously presented)The method of claim 15 wherein the step of increasing includes increasing an amplitude of the frequency.
17. (previously presented)The method of claim 16 wherein the step of increasing the amplitude includes injecting a signal to increase the amplitude of the frequency.